# NASA vicarious calibration of on-orbit ocean color satellite instruments

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## presentation outline

legacy of the NASA operational approach

general method

calibration of NIR (& SWIR) bands

calibration of visible bands

previous evaluations of alternative methods

### legacy of the NASA operational approach

H.R. Gordon, "In-orbit calibration strategy for ocean color sensors," Rem. Sens. Environ. 63, 265-278 (1998)

D.K. Clark et al., J. Geophys. Res. 102, 17209-17217 (1997) D.K. Clark et al., NASA Tech Merno. 2004-211632 (2003)

R.E. Eplee Jr. et al., "Calibration of SeaWiFS. II. Vicarious techniques," Appl. Opt. 40, 6701-6718 (2001)

B.A. Franz, et al., "Sensor-independent approach to the vicarious calibration of satellite ocean color radiometry," Appl. Opt. 46, 5068-5082 (2007).

P.J. Werdell et al., Appl. Opt. 46, 5649-5665 (2007) S.W. Bailey et al., Appl. Opt. 47, 2035-2045 (2008)

In place since SeaWiFS Reprocessing 4 (R2002)













## methods for gain estimation:

- $\label{eq:loss} \begin{array}{l} \mbox{slope & offset in lieu of ratio (~ slope with offset = 0)} \\ \mbox{gains calculated at $L_w$ in lieu of $L_t$} \\ \mbox{simultaneous use of $in situ aerosol optical thickness} \\ \mbox{zero Rayleigh (courtesy Zia Ahmad)} \\ \mbox{zero aerosol (no NIR contributions by aerosols or water)} \\ \mbox{NIR} \mbox{SWIR}; \mbox{SWIR} \mbox{NIR} \end{array}$

#### data sources

- modeled L\_u( $\lambda$ ) (Werdell et al. 2007) - alternative in situ data (NOMAD, BOUSSOLE; Bailey et al. 2008)

#### sensitivity analyses (Franz et al. 2007):

NIR-only calibration (no visible vicarious calibration)
 g(865) = 1.04 or 0.96 (+/- 4% from unity)
 alternative aerosol models





additional vicarious calibration info available from:

Sean Bailey Brvan Franz Zia Ahmad Chris Proctor Gene Eplee **Bob Barnes** 

http://oceancolor.gsfc.nasa.gov

Bource	-	Ń	412		63	490		510		555	670
MORY	D	66	1.0368	1.0	132	0.993		0.9982		0.9993	0.9729
64)			(0.009)	(0.0	295	(0.006	0	(800.00)		(0.009)	(0.007)
CV			1,736	1.7	73	1.61	£1 - 1	1.803		1.801	1.439
NOMAD		64	1.0395	1.0	135	0.994	97	0.9962		0.9969	0.9603
(a)			(0.013)		(0.013)		(0.034)			(0.013)	(0.009)
UPD			0.1300	0.0	1480	0.246	54	-0.1003		-0.0200	-0.1854
BOUSSOLE.		48	1.0402	1.0	129	0.996	31	1.0015		1.0007	0.9672
6.01			(0.005)	10.0	27)	(0.680	0	(0.031)		(0.021)	(0.006)
DPD			0.1831	-0.0	148	0.216	0	9.1600		0.0790	-0.2908
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Band Lucs(412)	N 154	107 *( apre M Retis 1.005	1.0401 D 0.3183 lain coeffici tral, COTS 0879 % Duff 11.762	1.0136 0.0395 ents for 3 instrume Table Rati	0.9969 0.3126 608Y da nL 9 9 6	0.9907 -0.4508 the process meMOBY 5 Doft 11.83	0.9958 -0.3502 ed to mimi m <sup>a</sup> Abs. UP 0.814	0.9691 -0.3906 ie a mult		00MAD/8002 % Diff 11-49	SSOLE Abs. UPD 0.713
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Band Lucs(412) Lucs(443) Lucs(400) Lucs(510) Lucs(510)	N 154 236 236 127	107 spec 30 Retio 1.005 0.918 0.918 0.953 0.953	1.0401 10 0.3183 lain coeffici tral, COTS 0897 11.762 15.96 13.62 11.97 1.97 1.97	1.0138 0.0395 enta for 3 instrume Table Rati 1.00 0.93 0.92 0.94	0.9949 0.3126 408Y da nt. • 5. Velo 6 6 6 9 9	0.9887 -0.4508 da process meMOBY 5 Diff 11.83 16.10 12.77 12.01 17.45	0.9958 -0.3502 ed to mimi m* Abs. UP 0.814 0.324 0.706 0.815 0.815	0.9601 -0.300 ic a mult c a mult	500 1997 1924 1933 1985	00MAD/B002 % Daff 11.49 16.32 12.74 12.26 22.95	SSOLE Als. UPD 0.713 0.313 1.235 1.636 1.639
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$\frac{\text{Band}}{L_{95}(412)}$ $\frac{L_{95}(443)}{L_{95}(510)}$ $\frac{L_{95}(550)}{L_{95}(550)}$ $\frac{L_{95}(550)}{C_{4}}$	N 154 236 236 127 236 233 383	10 10 100 100 0.918 0.953 0.963 0.961 1.779 1.001	1.0401 10 0.3160 lain coeffici trai, COTS 009Y % Diff 15.96 15.96 13.62 11.97 15.95 87.21 27.80	1.0138 0.0395 ents for 3 instrume Table Reti 1.00 0.93 0.92 0.94 0.55 1.21 0.58	0.9949 0.3126 fOBY de et. 5. Velo 6 6 6 8 9 9 8 8 0 8 8	0.9907 -0.4508 da process meMOBY 6 Deff 10.57 12.01 12.77 12.01 17.45 81.18 27.90	0.9958 -0.3502 ed to mini m* Abs. U7 0.814 0.324 0.706 0.815 1.223 1.269	0.902.0 001.0- ic a multi ic a mu	Latio 997 924 933 985 588 091 060	00MAD/BOC3 % Daff 11.49 16.32 19.74 19.26 16.25 85.49 29.42	SSOLE Als. UPT 0.713 0.313 1.235 1.636 1.572 1.542 3.636

